



# AirPrime XA1110 and XM1110

## Hardware Design Guide



**SIERRA**  
WIRELESS®

41111116  
Rev 3.0

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Due to the nature of wireless communications, transmission and reception of data can never be guaranteed. Data may be delayed, corrupted (i.e., have errors) or be totally lost. Although significant delays or losses of data are rare when wireless devices such as the Sierra Wireless modem are used in a normal manner with a well-constructed network, the Sierra Wireless modem should not be used in situations where failure to transmit or receive data could result in damage of any kind to the user or any other party, including but not limited to personal injury, death, or loss of property. Sierra Wireless accepts no responsibility for damages of any kind resulting from delays or errors in data transmitted or received using the Sierra Wireless modem, or for failure of the Sierra Wireless modem to transmit or receive such data.

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*Note: Some airlines may permit the use of cellular phones while the aircraft is on the ground and the door is open. Sierra Wireless modems may be used at this time.*

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## Revision History

Revision number	Release date	Changes
1	June 23, 2017	Initial draft in SWI template.
2	January 19, 2018	Updates throughout, changed title.
3.0	August 13, 2019	Removed obsolete module variants.

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# >> 1: Introduction

This document provides design guidelines for the following modules:

- Stand Alone GNSS module XM1110



Figure 1-1: XM1110 Multi-GNSS Module

- Integrated Patch Antenna Module: XA1110



Figure 1-2: XA1110

## Precautions

### **Please read carefully before you start**

If you use the GNSS receiver inside buildings, tunnels, or beside any huge objects, the GNSS signals might be cut-off or weakened. Please do not assume the receiver has malfunctioned.

This document provides the necessary guidelines for a successful system design using GNSS modules. For detailed module specifications, please refer to the corresponding datasheet of the GNSS module.

The GNSS module is an electrostatic sensitive device, please DO NOT touch the GPS module directly. Follow ESD safety rules when handling.

When using the device for the first time, it is strongly recommended that you test the device outdoors with open sky for at least 10 to 15 minutes to ensure that full ephemeris data is received.

## >> 2: General Rules for Design

This section provides rules to obtain the best performance when using the GNSS module.

### Circuit Design

#### Power Supply

A clean and stable power supply is required for the GNSS modules to perform optimally. An unstable power source will significantly impact GNSS performance. To achieve high-quality performance, the VCC ripple must be controlled under 50mVpp. Additional considerations to stabilize power supply include:

1. Adding a ferrite bead, power choke, or low pass filter for power noise reduction.
2. Adding a linear regulator (LDO) is rather than a switched DC/DC power supplier in the ripple.
3. Using enough decoupling capacitors with the VCC for stable voltage.

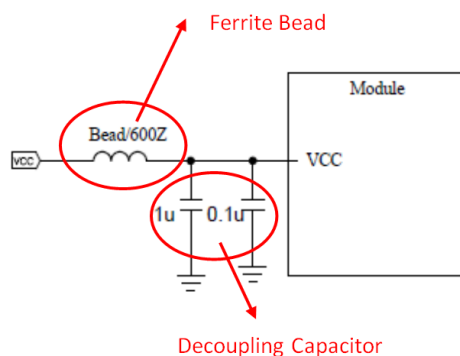


Figure 2-1: Power Design for the GNSS Module

#### VBACKUP Backup Battery

The GNSS module has a built-in charging circuit which charges the rechargeable coin battery.

It's recommended that the module be provided with backup power (e.g. Li-Ion rechargeable coin battery, super capacitor). See [Figure 2-2](#) for a reference design.

For information on the super capacitor reference design, please refer to [Super Capacitor Design](#).

Backup power is needed to maintain RTC operation and retain Ephemeris data in flash memory which helps the module get quicker TTFF and acquire PVT (Position, Velocity, Time) information.

If *VBACKUP* isn't connected to any coin battery, the GNSS module will execute a cold start each time it's restarted.

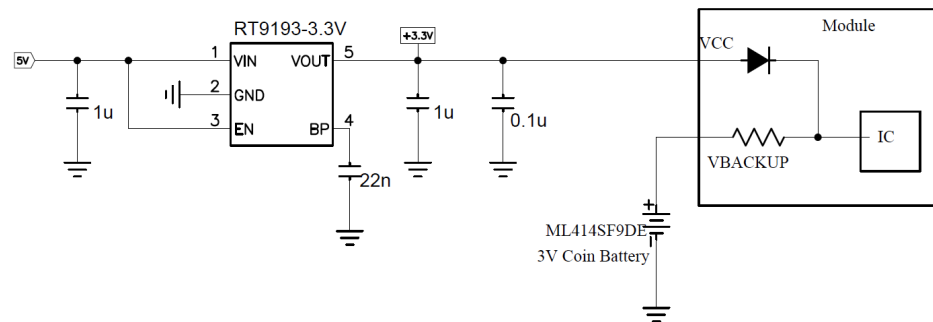


Figure 2-2: Rechargeable coin battery with VBACKUP

## UART / I<sup>2</sup>C/ SPI Serial Interface

### UART 0 (RX/TX)

1. UART is the TTL level interface that carries the baud rate ranging from 4800 bps to 115200 bps.
2. Placing a damping resistor on the RX and TX of the GNSS module could limit the interference from the host MCU or high speed digital logics. Fine tuning the damping resistor is required to efficiently suppress interference. The damping resistor is a wire-wound component and may function as a choke coil.
3. Don't connect diode(s) to RX/TX as it will decrease the signal driving capability which might adversely affect the RX/TX signal level. In some cases no data output will occur.
4. If RS232 logic-level is needed, a level shifter should be used. For more information please refer to [UART to RS232 Interface](#).
5. If USB logic-level is needed please refer to the [UART to USB Interface](#) design guidelines.

### I<sup>2</sup>C (SCL/SDA)

1. The I<sup>2</sup>C interface is usually connected to external devices. MT3333 supports only slave mode (default slave address is 0x10). MT3333 has 256 bytes of URAM mode and an 8-byte FIFO mode for transmitting and receiving data. The bit rate is up to 400 kb/s for fast mode. In addition, MT3333 supports a manual or automatic indicator for data transfer in the slave mode. Device addresses in slave mode are programmable.
2. A pull-up resistor must be added for the I<sup>2</sup>C bus:

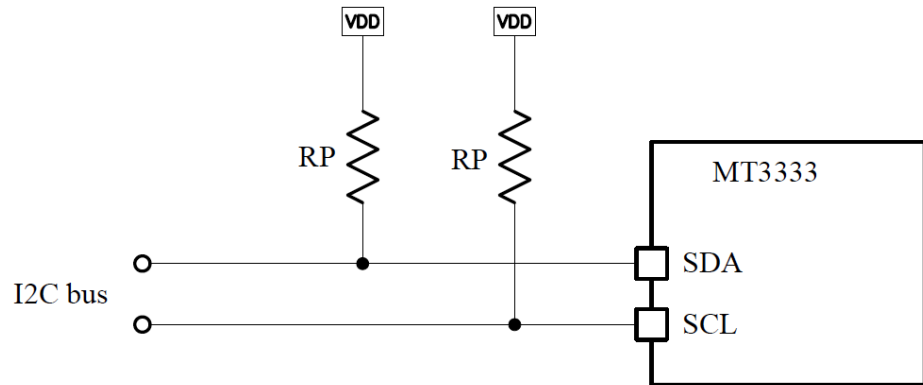


Figure 2-3: Addition of Pull-up Resistor

## SPI (CS/CLK/MISO/MOSI)

1. The serial peripheral interface port manages the communication between the digital BB and external devices. The MT3333 supports only slave mode. The slave has a 4 byte-register mode or *URAM* mode. In *URAM* mode, the size of the transmitted and received data is 256 bytes. The clock phase and clock polarity are selectable. The MT3333 supports a manual or automatic indicator for data transfer in slave mode. The bit rate is up to 700kb/s.

## Antenna Compliance Design

The GNSS antenna is the receiving part of the device that acquires weak GNSS signals from the sky. A common solution is to use a ceramic patch antenna because of its small form factor and low cost. There are two types of antennas: passive and active.

A *passive* antenna, is a standalone component without a signal amplifier such as an LNA. Patch antennas and chip antennas are the most commonly used passive antennas with GNSS modules. When using an external passive antenna, ensure that it is correctly fine-tuned for the specific module to ensure best possible signal strength.

An *Active* antenna is a standalone external antenna that comes with an integrated LNA. These antennas provide higher gain and better performance than that of a passive antenna. An example of an active antenna includes Patch Antenna with RF Cable and Integrated LNA.

Antenna should be chosen according to radiation efficiency, radiation pattern, gain, bandwidth, form factor, and cost. Make sure the ground plane is sufficient for the antenna to ensure best performance.

## Designing an External Passive Patch Antenna with GNSS module

1. In general, a 50Ω patch antenna will work well with the GNSS module. The antenna can be connected to the *Antenna IN* pin with a 50Ω impedance trace.
2. Please keep the patch antenna far away from noise sources such as the switching power supply and high speed digital logic and radar wave guide.
3. The 50Ω trace should be kept as short as possible to reduce the chance of picking up noise from the air and PCB. A simple direct-line trace is recommended.
4. If needed, a matching circuit can be placed between the patch antenna and the GNSS module. The matching circuit design should be discussed with the module and patch antenna manufacturer.
5. For 50Ω matching, please refer to [50 Ω Antenna Matching](#).

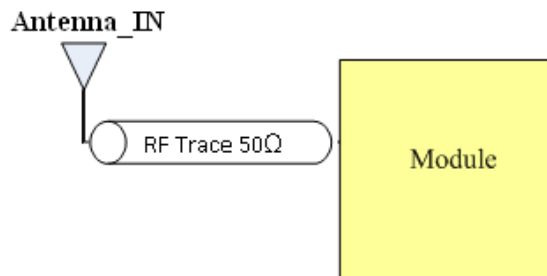


Figure 2-4: PCB Trace Design for Antenna Impedance Matching

## Selecting an Active Antenna Architecture for the GNSS Module

An external active antenna requires DC power in order to work properly. A typical method is to feed DC into the RF trace. The external antenna then extracts the DC from the RF trace. Thus the RF trace transports both the RF signal and DC power. An RF choke coil couples the DC power to the RF trace to perform this method.

Support two architectures for this as shown below in [Figure 2-5](#) and [Figure 2-6](#).

- **Mode1:** The power supply needs to be externally provided and is connected directly to the external antenna via a choke coil. See [Table 2-1](#).

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Note: Choke Coil for reference: LQG15HS33NJ02D (Murata)

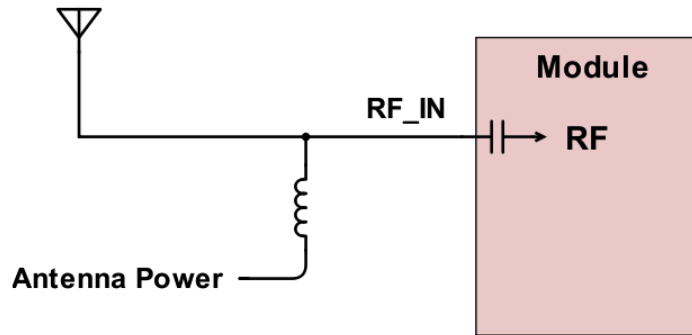
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- **Mode2:** The power supply for the external antenna needs to be externally fed into the module from the VCC pin directly and the antenna connected to the EX\_ANT pin.

**Table 2-1: Modes**

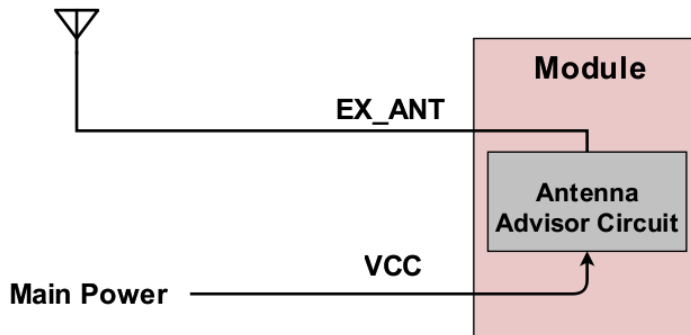
	XM1110	XA1110
<b>Mode 1 (via the VANT) (External Choke Coil)</b>	✓	
<b>Mode 2 (from the VCC) (Internal Choke Coil)</b>		✓

**External Antenna**



*Figure 2-5: Mode 1 (External Choke Coil)*

**External Antenna**



*Figure 2-6: Mode 2 (Internal Choke Coil)*

## Designing a Chip Antenna with GNSS Module

It's recommended to consult chip antenna vendors for more specific design guidelines. Below references are for chip antennas from *Pulse* and *Unictron*.

### 1. Pulse Antenna

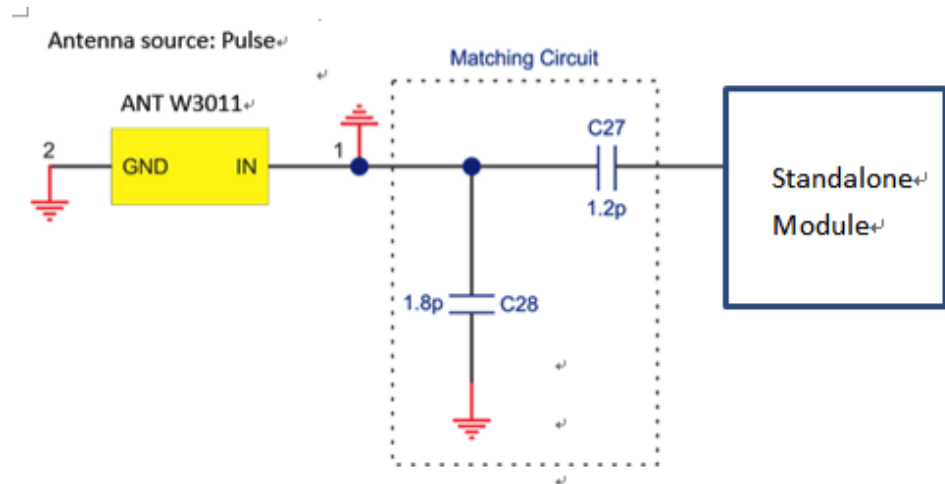


Figure 2-7: Pulse Schematic Design

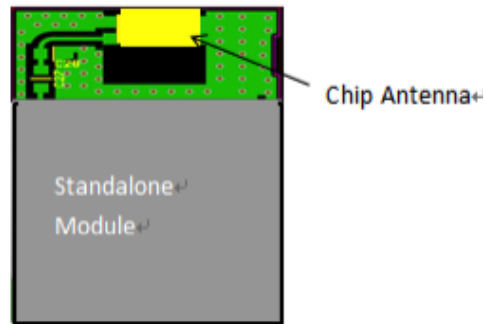


Figure 2-8: Pulse PCB Layout

Check antenna datasheet before tuning RF to match the component footprint (such as: C27, C28). You can base this on PCB size and housing to tune for an optimal value and meet the GNSS's frequency to get good reception.

Pulse web site:

[www.pulseeng.com/antennas](http://www.pulseeng.com/antennas)

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*Note: C27, C28's values are still based on your actual trace to tune it.*

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### 2. Unictron Antenna

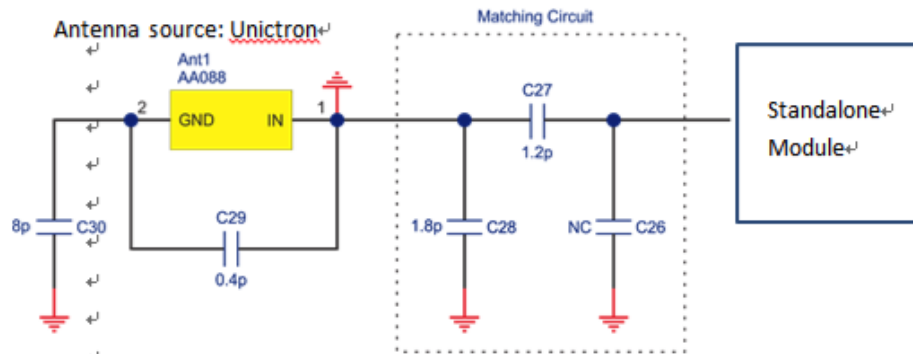


Figure 2-9: Unictron Schematic

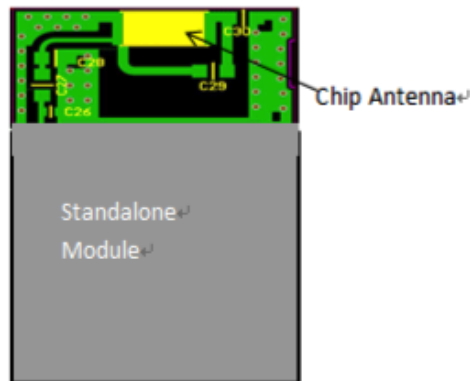


Figure 2-10: Unictron PCB

Check the antenna datasheet before tuning RF to match the component footprint (such as: C26, C27, C28, C29, C30). You can tune based on PCB size and housing to tune for an optimal value in order to meet the GNSS's frequency and for good reception.

Unictron web site: <http://www.unictron.com/index/>

Note: The values for C26, C27, C28, C29, and C30 are tuned based on your trace.

## External Antenna of Specification

When selecting your external antenna, refer to the specification shown in Table 2-2 and Table 2-3 below.

Table 2-2: GPS/GLONASS External Antenna

Characteristic	Specification
Polarization	Right-hand circular polarized
Frequency Received	1.575GHz~1.615GHz

Table 2-2: GPS/GLONASS External Antenna (Continued)

Characteristic	Specification
Power Supply	3.3V
DC Current	5mA<IDC<11mA at 3.3V
Total Gain	27±3dB
Output VSWR	2.0
Impedence	50Ω
Noise Figure	2dB

Table 2-3: Beidou/GPS External Antenna

Characteristic	Specification
Polarization	Right-hand circular polarized
Frequency Received	1.561GHz~1.575GHz
Power Supply	3.3V
DC Current	3mA<IDC<30mA at 3.3V
Total Gain	27±1dB
Output VSWR	2.0
Impedence	50Ω
Noise Figure	1.5dB

## 1PPS

1PPS signal is an output pulse signal used for timing applications. Its electrical characteristics are:

- Low Voltage level: 0~0.4V
- High Voltage level: 2.8~3.1V
- Period: 1s
- Accuracy (jitter):±20ns
- 100ms pulse width duration

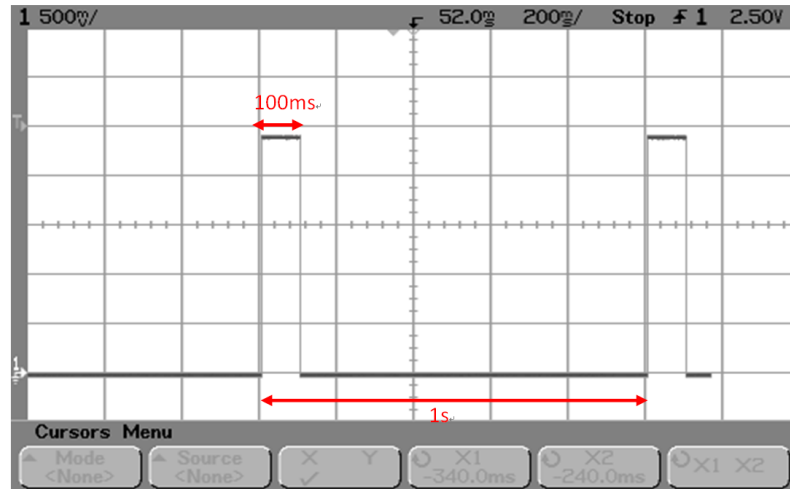


Figure 2-11: 1PPS signal and its pulse width with 100ms duration

## Free run 1PPS Output Before 3D\_FIX

The Sierra Wireless standard GNSS module outputs 1PPS signal after the module obtains a 3D\_FIX. This is a factory default setting.

## Cable Delay Compensation

In some cases, a long-distance connection (~300m) may be needed. For a timing application, the cable length is critical. For more information on 1PPS signal transmission delay please refer to [How to Efficiently Transfer 1PPS Through Extended Distances](#).

## LED Indicator for 1PPS Signal

For 1PPS LED indication, you may connect an LED indicator with a 330ohm resistor in series.

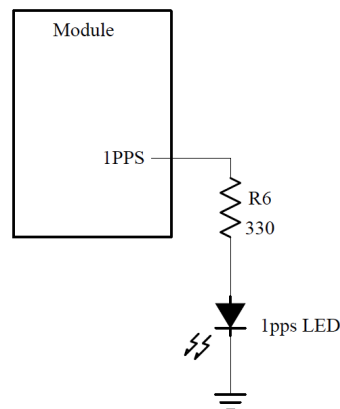


Figure 2-12: 1PPS Signal Design for IO

## 1.8V Boost to 3.3V Application

If you want to use the 3.3V's GNSS module in a 1.8V system there are two considerations: power supply translation and signal level shift. For power supply translation, you can use a boost circuit which can boost 1.8V to 3.3V (refer to [Figure 2-13](#) below).

TPS61097A-33 is the TI's boost IC which can support boost functionality. In its application C1 and C2 need to use 10uF and L1 is 10uH. It can support approximately 100mA of output. For information about the capacitor and inductor's placement, refer to the application note on the TI web site: <http://www.ti.com/lit/ds/symlink/tps61097a-33.pdf>.

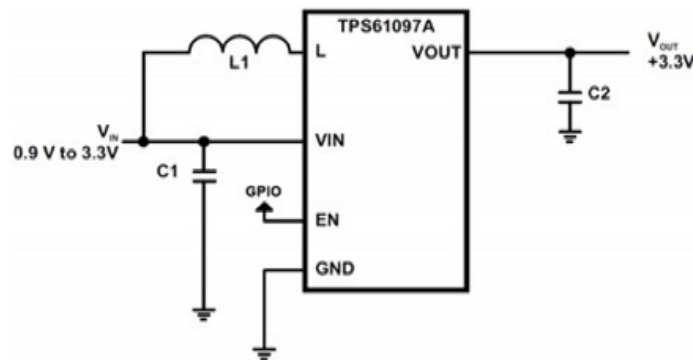


Figure 2-13: Application Schematic for TI Boost IC

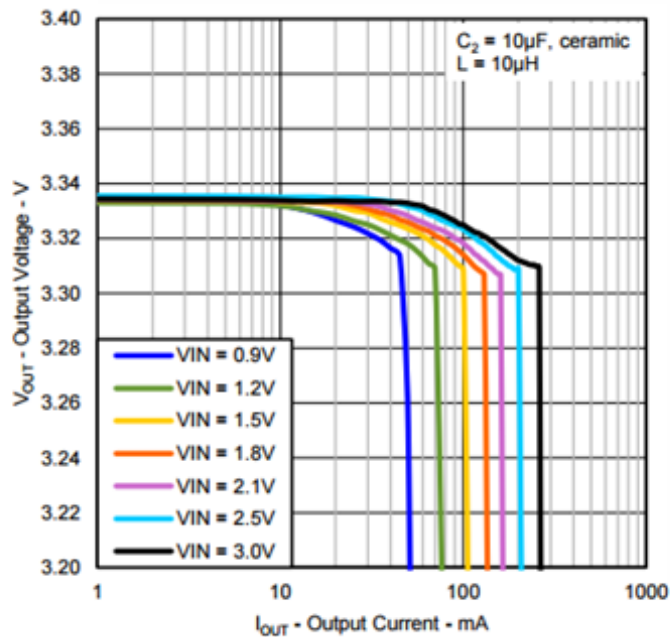


Figure 2-14: Output Voltage vs Output Current

For signal level shift, when your host system is 1.8V and the Sierra Wireless module is 3.3V, the host system can control the Sierra Wireless module by using a signal level shift circuit (refer to [Figure 2-15](#) below). R1 to R4's values are default values. In your design, you can adjust their values to achieve control. The 2N7002L can select low RDS(On) to reduce power consumption through a voltage drop.

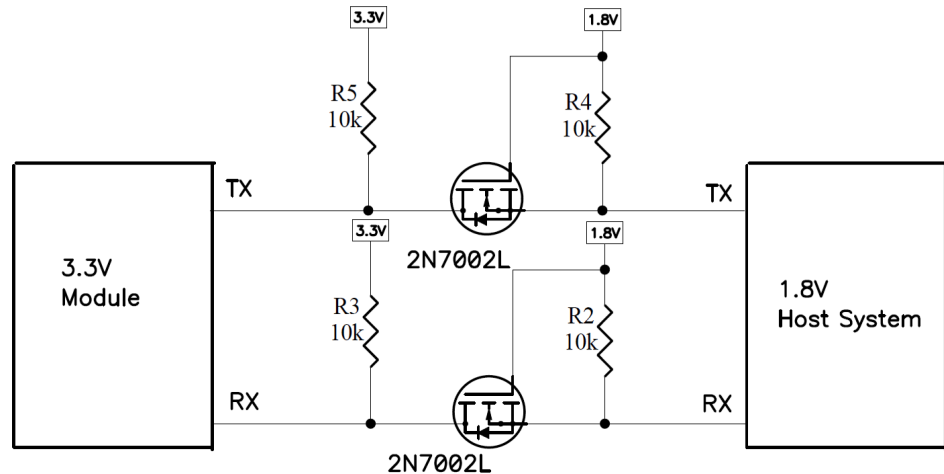


Figure 2-15: Signal Level Shift Circuit

## Layout Guidelines

Please follow the layout guidelines during the design process.

## Layout Underneath the GNSS Module

In general, GNSS modules have high receiving sensitivity at around -165dBm. During hardware integration, try to avoid noise or harmonics in the following bands to prevent unnecessary reception degradation:

- Beidou 1561.098MHz  $\pm$ 2.046MHz and GPS 1572.42MHz $\pm$ 2MHz
- GLONASS 1598.0625~1605.375MHz

Modern GNSS positioning products include many components such as an LCD screen, MCU, high speed digital signal (access memory card), and an RF system (i.e. Cellular module, BT, Wi-Fi, DVB-T). Keep these components away from the GNSS module to avoid noise interference, otherwise it may result in poor GNSS RF reception.

## For XM1110

Don't leave any trace or mark underneath the GNSS module as indicated by the circled area in figure [Figure 2-16](#) below.



## Keep XA1110 Far Away from High Profile or Metal-Canned Components

It's good practice to place the GNSS module far away from any high-profile components especially those enclosed in metal cases such as the E-CAP, coin battery, and Pin Header. The antenna field pattern can be affected, and pattern distortion can occur. At worst, this will decrease the GNSS signal up to ~10dB.



Figure 2-18: First Example of Bad and Good GNSS Module Placement

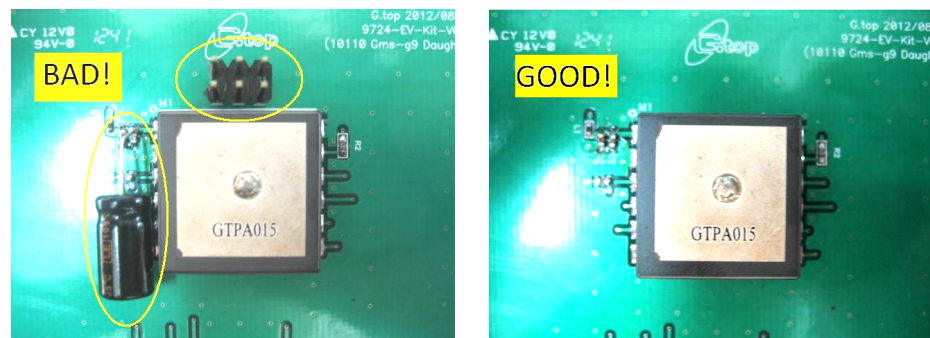


Figure 2-19: Second Example of Bad and Good GNSS Module Placement

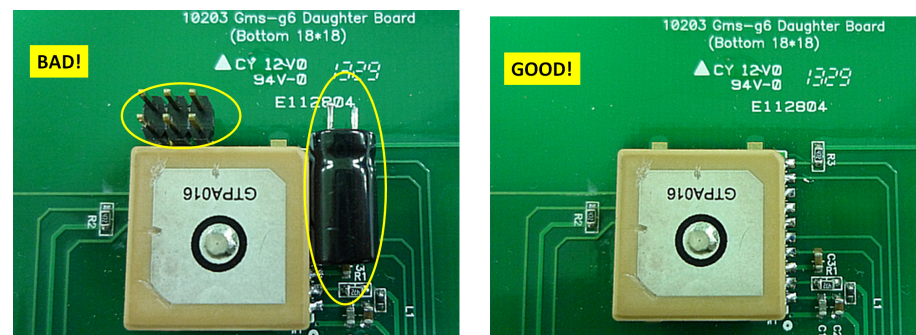


Figure 2-20: Third Example of Bad and Good GNSS Module Placement

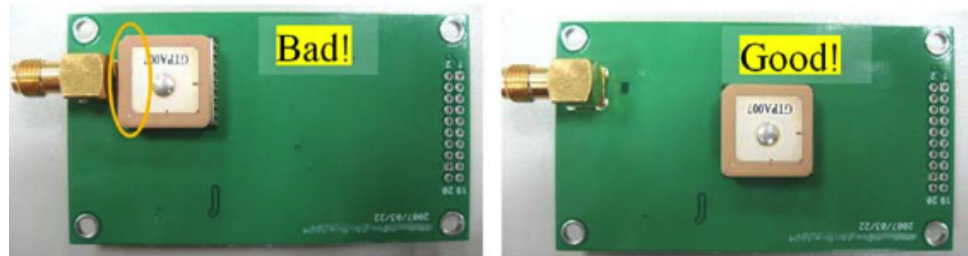


Figure 2-21: Example of Bad GPS Module Placement (Patch Antenna Close to a High-Profile Metal Case Component) and Good Placement

## Placement

- Place the decoupling capacitors for the *VCC* close to the GNSS module.
- Place the damping resistors for *TX/RX* close to GNSS module.

### Do not place the GNSS module:

- in proximity to high-speed digital processing circuitry
- in proximity to high-current switching power circuitry
- in proximity to clock sources circuitry

## Trace

1. The USB differential signals should be traced closely and be of equal length for better noise immunity and minimum radiation.
2. Apply a 50 ohm impedance RF trace for correct impedance matching.
3. Any right angle turn in trace routing should be done with two 135 degree turns or an arc turn.

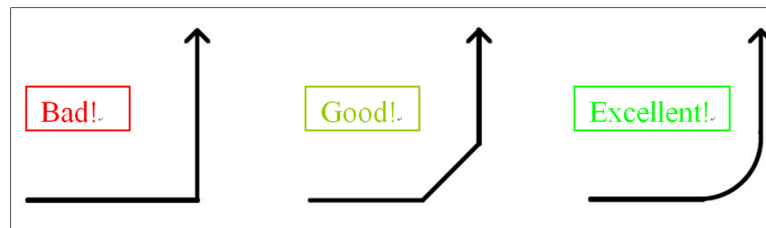


Figure 2-22: Examples of turns in trace routing

It is better to have an independent trace of the power source for all components:

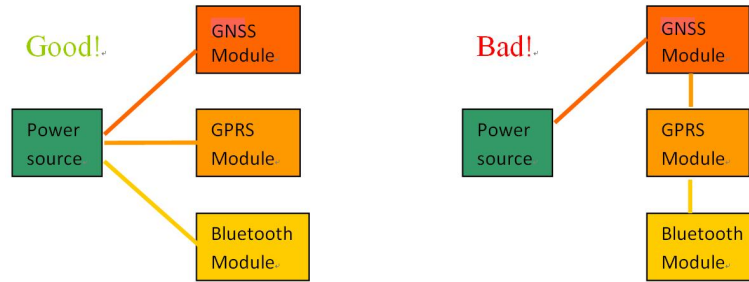


Figure 2-23: Examples of Independent Trace

## Ground Segmentation

In general, the separation of ground between the GPS module and the rest of the system is recommended to avoid interference. If this is not possible, it is best to follow these rules: segmentation of ground between digital and analogue system, high current and low current system, and different radiation systems such as GPS and GPRS.

One way to segment the ground is to place digital and noise components at one corner of the board, while placing analog and quiet components at the opposite corner of the board. Make sure there is no crossing of microstrip or current between the two component sets with ground; each set is to be contacted to one point only.

Another method is to place the two different sets at different layers of the board, while the ground of each layer is contacted at one point only which is ideally located at the border of the board.

## Ground Plane for XA1110

A large GND plane directly underneath the module can enhance the magnetic-field line of the antenna for better GNSS signal reception. Typically it will improve reception by up to ~2dB. It is strongly recommended that the ground plane underneath the GNSS module be as large as possible.

The recommended thickness for the ground layer is 0.5 to 1 OZ (0.0175 to 0.035 mm). It is best to place the ground plane on the top layer of the PCB, directly underneath the GNSS module as shown in [Figure 2-24](#).

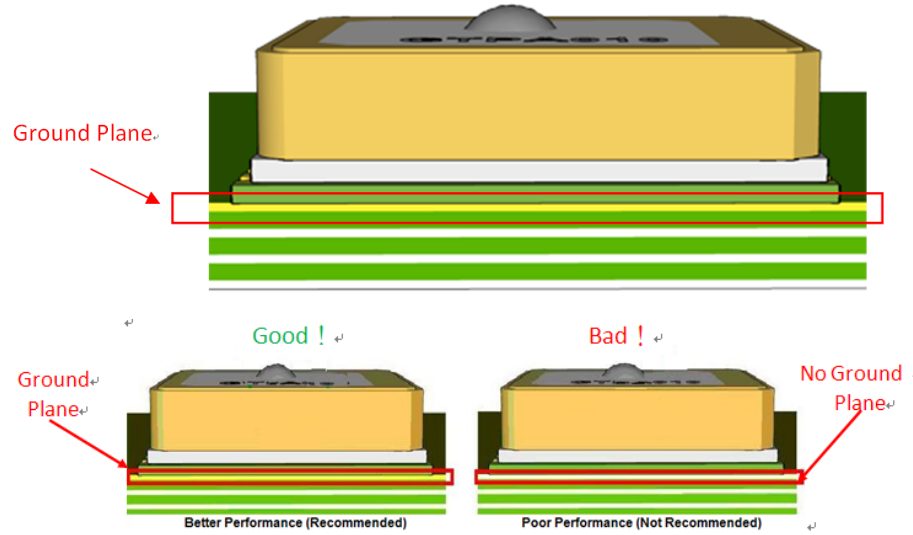


Figure 2-24: Ground Plane for FR4 Design

## 3: Thermal Profile for SMD Modules

The following information is Pb-Free compliant. The details are for reference only.

### SMT Reflow Soldering Temperature Profile

- Solder paste alloy: SAC305 (Sn96.5/Ag3.0/Cu0.5).
- Pre-heat Temp: 150–200°C; Soak time ( $t_s$ ): 60–120sec.
- Peak temp ( $T_p$ )  $\leq$  250°C.
- Time above 220°C ( $t_p$ ): 40–90sec.
- Optimal cooling rate  $< 3^\circ\text{C}/\text{sec}$ , from peak to 220°C.
- The oxygen concentration  $< 2000$  ppm.

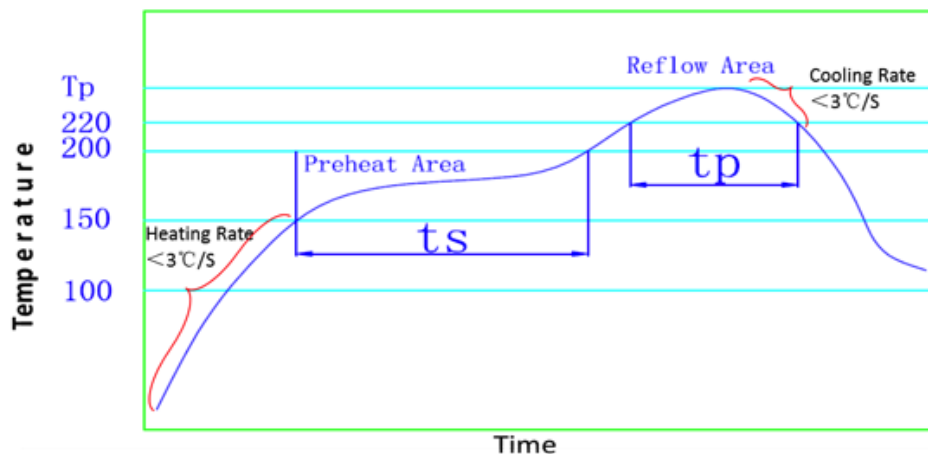


Figure 3-1: SMT Reflow Soldering Temperature Profile

### SMT Solder Mask

Using the dimensions of the PCB pad as a reference, subtract the size by 0.1 to 0.2 mm and use that as a layout for the paste mask (for a PCB pad layout, please see “Recommended PCB pad layout” on the individual GPS module data sheet).

### Manual Soldering

Soldering iron: Bit Temperature: under  $380^\circ\text{C}$  | Time: under 3 seconds.

## >> 4: Troubleshooting

### How to Check the Working Status of the GPS Module

The first thing to check for is the NMEA sentence output through *TX* using various application tools. For example: you may use the Windows tool: *HyperTerminal* or you may use another GPS application program.

If there is no NMEA output at the *TX* pin, this indicates that the module is currently not working. Please double check your schematic design. The following is a list of possible items to check:

#### Item 1: VCC

The voltage should be kept between 3V to 4.3V (typical: 3.3V).

#### Item 2: VBACKUP

The voltage should be kept between 2.0V and 4.3V (typical: 3.0V). If a backup battery is not installed for the *VBACKUP* pin, the pin could still be measured as the voltage comes from the built-in battery recharging circuit. It is recommended that power be provided to the *VBACKUP* pin as it is used to keep the RTC time running and to preserve stored navigation data.

#### Item 3: TX0

The UART transmitter of the module outputs the GPS NMEA information for the application.

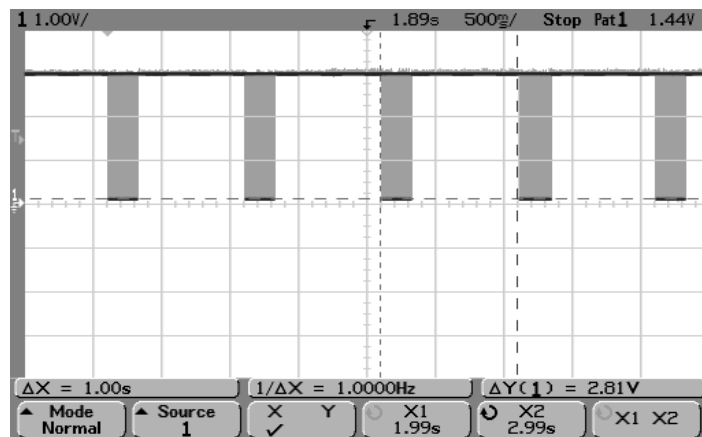


Figure 4-1: TX0

# >> | Appendix A: Super Capacitor Design

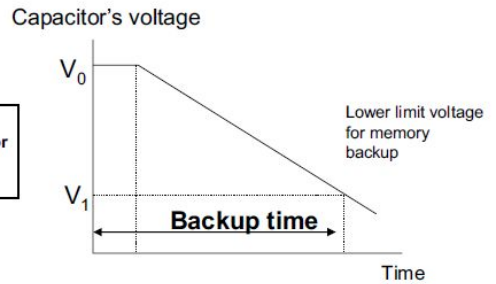
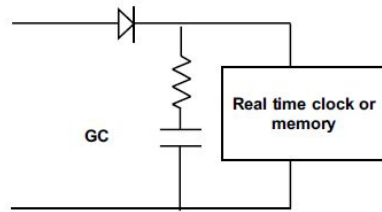
## About Super Capacitors

Super capacitors have a lifetime similar to that of aluminum electrolytic capacitors. The service life of a super capacitor is greatly dependent on the operating temperature, humidity, applied voltage, current, and backup time. Therefore, the service life is determined based on the backup time set by the customer.

## How to Calculate the Backup Time

The example below shows how to calculate the backup time:

$$T = C (V_0 - V_1) / (I + I_L)$$



**Example:**

$$V_0 = 2.5V, V_1 = 1.8V, I = 10\mu A, C = 0.2F$$

$$T = 0.2 ( 2.5 - 1.8 ) / ( 10 \text{ e-}6 + 0.2 \times 10^{-6} )$$

$$= 0.14 / 10.2 \times 10^{-6}$$

$$= 13,725 \text{ seconds}$$

$$= 3.8 \text{ hours}$$

- T: Backup time (second)
- C: Capacitance of Gold Capacitor (F)
- $V_0$ : Applied voltage(V)
- $V_1$ : Lower limit voltage for memory backup(V)
- I: Current during backup(A)
- $I_L$ : Leakage current(A) about 0.2 $\mu$ A

Figure A-1: Calculating Backup Time

## >> Appendix B: 50 Ω Antenna Matching

We used the *AppCAD* tool to simulate 50Ω impedance for the RF PCB layout.

**Table B-1: Antenna Matching**

RF Line Width (W)	PCB FR4 Thickness	Dielectric Parameters	Copper Thickness per ounce
1.8mm	1mm	4.6	0.035mm

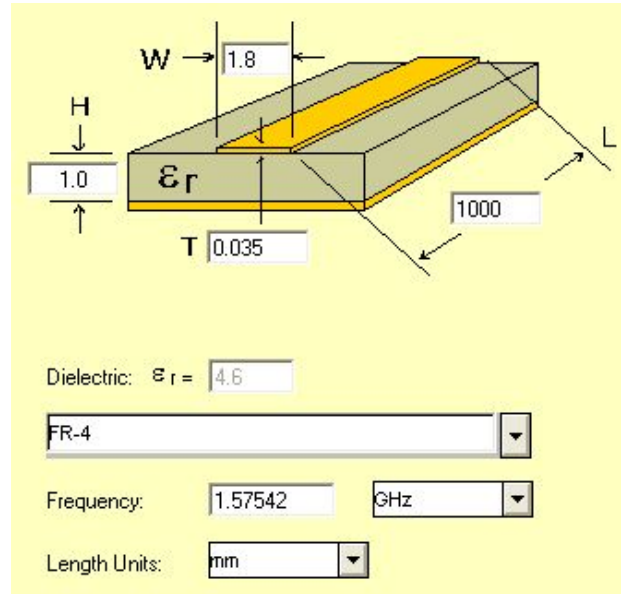


Figure B-1: Dimensions

**Notice:**

For multi-layer layouts, you can place a ground layer in the second layer to minimize the trace width in a specific PCB (such as FR4) and impedance.

For impedance calculation, there is free software available to calculate the trace width or impedance. Once such software package is:

<http://www.awrcorp.com/products/additional-products/tx-line-transmission-line-calculator>

# >> Appendix C: UART to RS232 Interface

Typically, an RS232 or USB interface is required to connect the PC to the Sierra Wireless GNSS module for communication. Most Sierra Wireless modules use a set of communication ports in TTL-logic. A bridge IC may be needed for RS232 signal conversion.

The supported baud-rates are 4800, 9600, 14400, 19200, 38400, 57600, and 115200 bps.

Please refer to the reference circuit in [Figure C-1](#) below for RS232 signal conversion. An SP3320 IC is used here as an example.

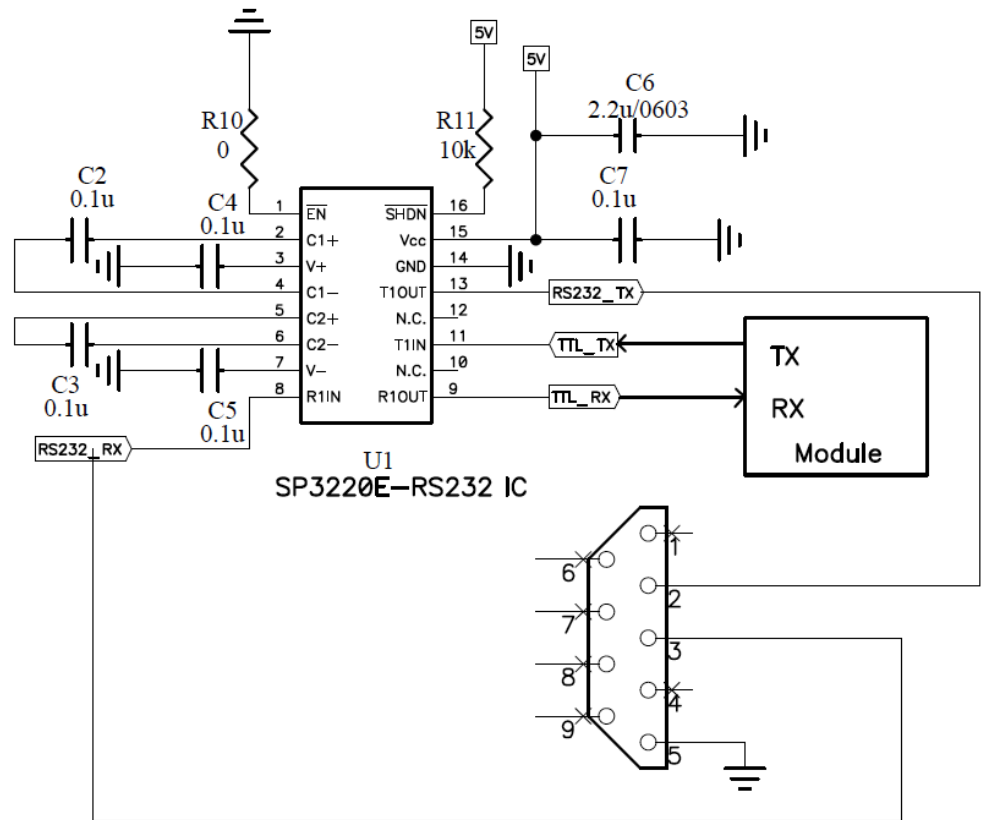


Figure C-1: RS232 Signal Conversion Example



## >> Appendix E: How to Efficiently Transfer 1PPS Through Extended Distances

There are several aspects to note when transferring a 1PPS signal through a long cable which will result in a 1PPS signal degradation, an increase in noise, and an increase in signal delay. As the 1PPS signal is traveling through the communication cable, impedance matching must be implemented to prevent waveform distortion. Depending on your application, an OP-amp can be added to control the accuracy of the voltage level for the 1PPS signal.

When using a 1PPS signal for time synchronization, the OP-amp chosen should have a high slew rate property to prevent a large delay in the 1PPS. The accuracy level of 1PPS for Sierra Wireless GNSS modules is within 100ns. This applies to most of Sierra Wireless' MTK GNSS modules. The reference design in [Figure E-1](#) below can be used to improve accuracy to within 80ns.

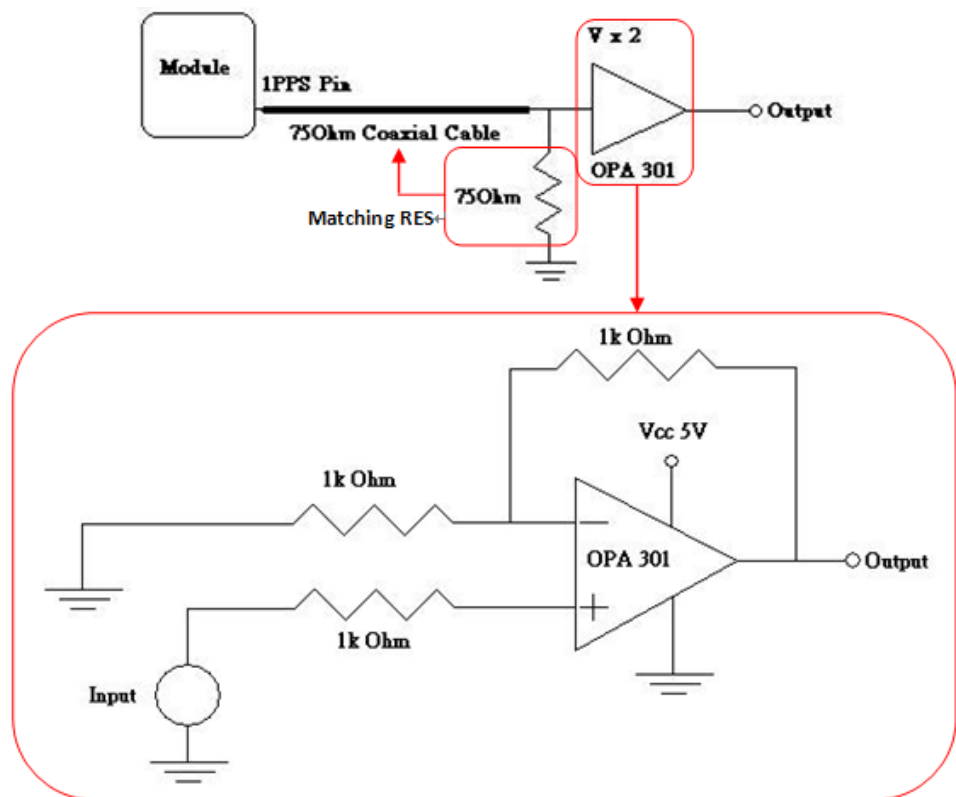


Figure E-1: Design to Improve Accuracy to within 80ns

# 1pps Delay Time

When using coaxial cable for long distance communication using an OP-amp for amplification, pay close attention to the coaxial cable time delay and the rising time of the wave form due to the OP-amp’s slew rate. A brief explanation for this is given below.

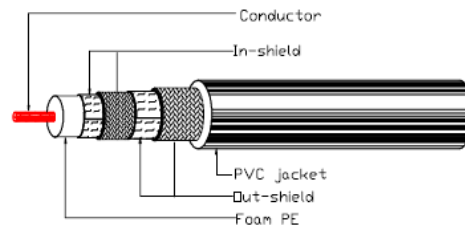
Figure E-2 shows the specification of the coaxial cable with the model number RG6U.

## CONSTRUCTION

Item		A.Q.L.	Description
Conductor	No./mm	1.02 (± 0.025)	Copper clad steel
	1.02 CCS		
Insulation	No./mm	4.57 (± 0.20)	Foamed PE insulation
	4.57		
Shield	B-APA	64 (±2); 0.16 (± 0.01)	Bonded double aluminium foil shield
	64/0.16(AL)		Aluminium wire braid shield
	APA		Double aluminium foil shield
	48/0.16(AL)		Aluminium wire braid shield
Jacket	No./mm	7.20 (± 0.30)	Black flame retardant PVC jacket
	7.20 PVC		

Figure E-2: RG6U Specifications

## DESIGN



## CHARACTERISTICS

ITEM	Description	Standards	
Conductor Resistance	20°C, conductor DC resistance	<10Ω/100M	
Capacitance		53.2 ± 5pF/M	
Velocity Ratio		83 ± 3%	
Characteristic Impedance	20°C, 200MHz	75Ω ± 3Ω	
Return Loss	20°C, 5 --- 200MHz	>20dB	
Attenuation	20°C -dB/100M (± 10%)	55MHz	4.94
		211MHz	9.43
		400MHz	13.12
		870MHz	19.99
		1000MHz	21.46
		2000MHz	31.82

Figure E-3: RG6U Design and Characteristics

## The Delay Time Caused by the Cable

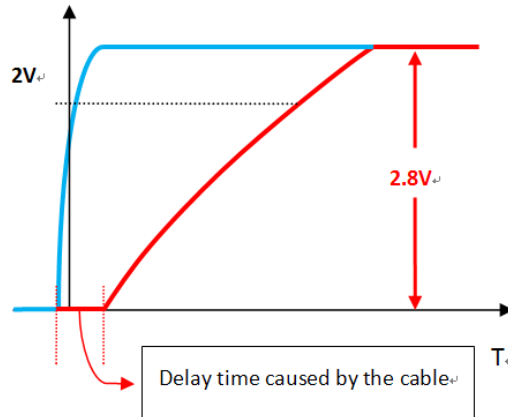


Figure E-4: Delay Time Caused by the Cable

## Calculating the Delay Time in Respect to the Communication Cable Length

The simplest method to calculate this is to have a good grasp of the relationship of the three parameters:

1. The speed of the traveling waveform.
2. The distance of the wave form traveled.
3. The delay time.

$$\frac{\ell}{\mu_p} = T$$

$\ell$  = Distance of the wave form traveled (m)

$\mu_p$  = Speed of the waveform (m/s)

$T$  = Delay Time (ns)

If the speed of the waveform (in the coaxial cable) is unknown, it is possible to use a known coaxial cable length to test. For example, the signal travel in one meter of coaxial cable may have a delay time measured by an oscilloscope as 5ns and consequently the  $\mu_p$  will be  $2 * 10^8$  (m/s).

If the value of capacitance and inductance for the coaxial cable is known, then  $\mu_p$  (m/s) can also be calculated.

$$\frac{1}{\sqrt{LC}}$$

Other coaxial cable electromagnetic fundamental parameters along with the inner and outer diameter of the physical cable can be used in combination to perform theoretical calculations.

## Waveform Rising Time Caused by OP-amp

Figure E-5 shows the slew rate which is the time needed for a rising waveform. When the SR ( $V/\mu\text{sec}$ ) of OPA is higher, the rising time will be shortened as well.

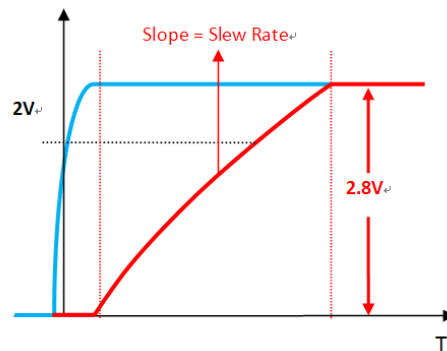


Figure E-5: Slew Rate

## Recommended OP-amp

If an inadequate OP-amp is chosen (i.e. with a low slew rate), the delay at the rising time introduced to the waveform can be significantly larger than that of the coaxial wire.

We recommend using OP-amp 301 to decrease the waveform rising time.

Specification of OP-amp 301:

- Low Power: 9.5mA (Typ) on 5.5V
- Single Power: 2.7V ~ 5.5V
- High Slew Rate: 80 V/sec
- Tiny Packages: MSOP and SOT23

## Voltage Degradation of Communication Cable

Tests with a 10m long coaxial cable showed an insignificant amount of voltage degradation. Users should not be concerned with this issue.

# >> Appendix F: Reflow Soldering Precautions

**Table F-1: Precautions**

	Details	Suggestions	Notes
1	Before proceeding with the reflow-soldering process, the GPS module must be pre-baked.	Pre-bake Time: 6 Hours @ 60°±5°C or 4 Hours @ 70°±5°C	The maximum tolerated temperature for the tray is 100°C.  After the pre-baking process, please make sure the temperature is sufficiently cooled down to 35°C or below in order to prevent any tape and reel deformation.
2	Because PCBA (along with the patch antenna) is highly endothermic during the reflow-soldering process, extra care must be taken with the GPS module's solder joint for any signs of cold welding or false welding.	The parameters of the reflow temperature must be set accordingly to module's reflow-soldering temperature profile.	Double check to see if the surrounding components around the GPS module are displaying symptoms of cold welding or false welding.
3	Special attention is needed for the PCBA board during reflow-soldering to see if there are any symptoms of bending or deformation to the PCBA board, possibly due to the weight of the module. If so, this will cause concerns at the latter half of the production process.	A loading carrier fixture must be used with PCBA if the reflow soldering process is using rail conveyors for the production.	If there is any bending or deformation to the PCBA boards, this might cause them to collide into one another during the unloading process.
4	Before the PCBA undergoes a reflow-soldering process, the production operators must visually check to see if there are positional offsets to the module, because it will be difficult to readjust after the module has gone through the reflow-soldering process.	The operators must visually check and readjust the position before the reflow-soldering process.	If the operator is planning to readjust the module position, please do not touch the patch antenna while the module is hot in order to prevent a rotational offset between the patch antenna and module.

**Table F-1: Precautions**

	Details	Suggestions	Notes
5	<p>Before handling the PCBA, they must be cooled to 35°C or below after they have undergone a reflow-soldering process, in order to prevent a positional shift which may occur when the module is still hot.</p>	<ol style="list-style-type: none"> <li>1. You may use an electric fan behind the reflow machine to cool them down.</li> <li>2. Cooling the PCBA can prevent the module from shifting due to fluid effect.</li> </ol>	<p>It is very easy to cause a positional offset to the module and its patch antenna when handling the PCBA under high temperatures.</p>
6	<ol style="list-style-type: none"> <li>1. When separating the PCBA panel into individual pieces using the V-Cut process, special attention is needed to ensure that there are sufficient gaps between patch antennas.</li> <li>2. If the V-Cut process is not available and the pieces must be separated manually, please make sure the operators are not using excess force which may cause a rotational offset to the patch antennas.</li> </ol>	<ol style="list-style-type: none"> <li>1. The blade and the patch antenna must have a gap greater than 0.6mm.</li> <li>2. Do not use the patch antenna as the leverage point when separating the panels by hand.</li> </ol>	<ol style="list-style-type: none"> <li>1. Tests must first be performed to determine if the V-Cut process is going to be used. Ensure that there is enough space between the blade and patch antenna so that they do not touch one another.</li> <li>2. An uneven amount of manual force applied to the separation will likely to cause a positional shift in the patch antenna and module.</li> </ol>
7	<p>When separating the panel into individual pieces during latter half of the production process, special attention is needed to ensure the patch antennas do not come in contact with one another in order to prevent chipped corners or positional shifts.</p>	<p>Use a tray to separate the individual pieces.</p>	<p>It is possible to chip a corner and/or cause a shift in position if the patch antennas come into contact with each other.</p>

## Other Cautionary Notes on the Reflow-Soldering Process

1. Module must be pre-baked **before** going through the SMT solder reflow process.
2. The usage of solder paste should follow the “First-in-First-out” principle. Opened solder paste needs to be monitored and recorded in a timely manner (refer to IPQC standards for related documentation and examples).
3. Temperature and humidity must be controlled within an SMT production line and storage area. A temperature of 23°C, 60±5% RH humidity is recommended (please refer to IPQC standards for related documentation and examples).
4. When performing solder paste printing, check if the amount of solder paste is in excess or insufficient, as both conditions may lead to defects such as electrical shortage, empty solder, and etc.
5. Make sure the vacuum mouthpiece is able to bear the weight of the GPS module in order to prevent a positional shift during the loading process.
6. Before the PCBA goes through the reflow-soldering process, the operators should check by his/her own eyes to see if there is a positional offset to the module.
7. The reflow temperature and its profile data must be measured before the SMT process and match the levels and guidelines set by IPQC.
8. If an SMT protection line is running a double-sided process for PCBA, please process the GPS module during the second pass only to avoid repeated reflow exposures of the GPS module. Please contact Sierra Wireless beforehand if you must process the GPS module during the first pass of double-side process.

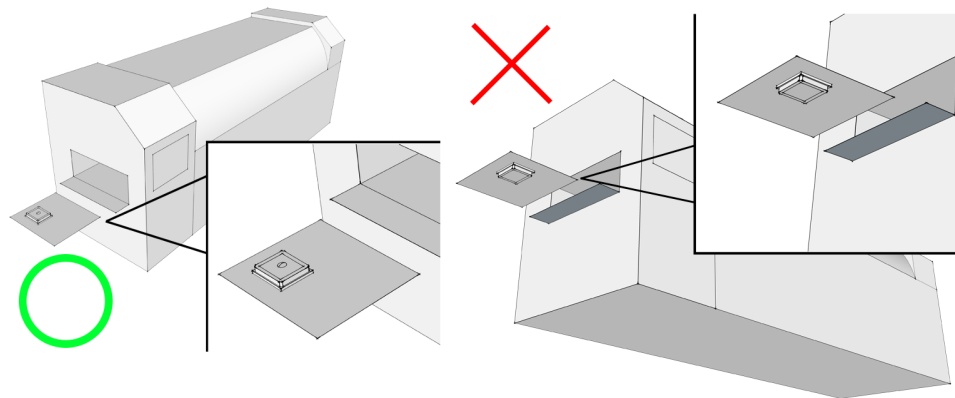


Figure F-1: Placing the GPS module right-side up when running the reflow-solder process; do not invert.

## Manual Soldering

### Soldering Iron

Heat Temperature: Under 380°C | Time: Under 3 sec.

**Notes:**

1. To prevent further oxidation, do not directly touch the soldering pads on the surface of the PCB board.
2. The solder paste must be defrosted to room temperature before use so that it can return to its optimal working temperature. The time required for this procedure is unique and dependent on the properties of the solder paste used.
3. The steel plate must be properly assessed before and after use, so its measurement stays strictly within the specification set by SOP.
4. Watch out for the spacing between the soldering joints, as excess solder may cause electrical shortages.
5. Exercise caution and do not use an excessive amount of flux due to possible siphon effects on neighboring components, which may lead to electrical shortages.
6. Do not use a heat gun for long periods of time when removing the shielding or inner components of the GPS module, as it is very likely to cause a shift to the inner components which will lead to electrical shortages.